

# Directional Dipole Model for Subsurface Scattering

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Rendering translucent materials using Monte Carlo ray tracing is computationally expensive due to a large number of subsurface scattering events. Faster approaches are based on analytical models derived from diffusion theory. While such analytical models are efficient, they miss out on some translucency effects in the rendered result. We present an improved analytical model for subsurface scattering which captures translucency effects that are present in the reference solutions but remain absent with existing models. The key difference is that our model is based on ray source diffusion, rather than point source diffusion. A ray source corresponds better to the light that refracts through the surface of a translucent material. Using this ray source, we are able to take the direction of the incident light ray and the direction toward the point of emergence into account. We use a dipole construction similar to that of the standard dipole model, but we now have positive and negative ray sources with a mirrored pair of directions. Our model is as computationally efficient as existing models while it includes single scattering without relying on a separate Monte Carlo simulation, and the rendered images are significantly closer to the references. Unlike some previous work, our model is fully analytic and requires no precomputation.

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## 1. INTRODUCTION

Rendering of translucent materials, such as skin, foods, minerals, and many other natural materials, has many important use cases in computer graphics. For more than a decade, the dipole approximation for subsurface scattering [Jensen et al. 2001] has proven to be a fast practical way of rendering such materials. This standard dipole model is however built upon a number of assumptions which are often violated. One significant assumption is that incident light is directionally uniform. This assumption is evident from the fact that the standard dipole model is a function only of the distance between the point of incidence and the point of emergence. The same assumption has been used in recently introduced analytical models [d'Eon and Irving 2011]. The lighting distribution in realistic scene configurations, however, is rarely directionally uniform.

We introduce a directional dipole model for subsurface scattering which produces images that are closer to path traced references. Our model is a fully analytical BSSRDF that does not assume directionally uniform incident illumination. The derivation of our model is based on a new analytical solution to the diffusion equation for a ray of light in a highly scattering medium with infinite extent [Menon et al. 2005a; 2005b]. To handle boundary conditions, we extend this ray source solution to a dipole construction, namely a mirrored pair of directional sources. This construction is inspired by the standard dipole model [Jensen et al. 2001].

Conventionally, single scattering is separated out from a model for subsurface scattering. The ray source we use enables us to include approximate single scattering in our model. We can thereby evaluate complete subsurface scattering effects without relying on a separate, potentially costly evaluation of single scattering based on Monte Carlo ray tracing. Thus, while our inclusion of directional effects adds some costs in a rendering, the inclusion of single scattering balances these additional expenses, and outweighs them when light sources are small (or singular). Figure 1 highlights our results.

## 2. RELATED WORK

The most general approach for rendering participating media is to solve the radiative transfer equation by Monte Carlo ray tracing (*path tracing*) [Rushmeier 1988]. This approach becomes extremely costly for highly scattering media, where the average number of scattering events (and thus the number of rays to be traced) is very

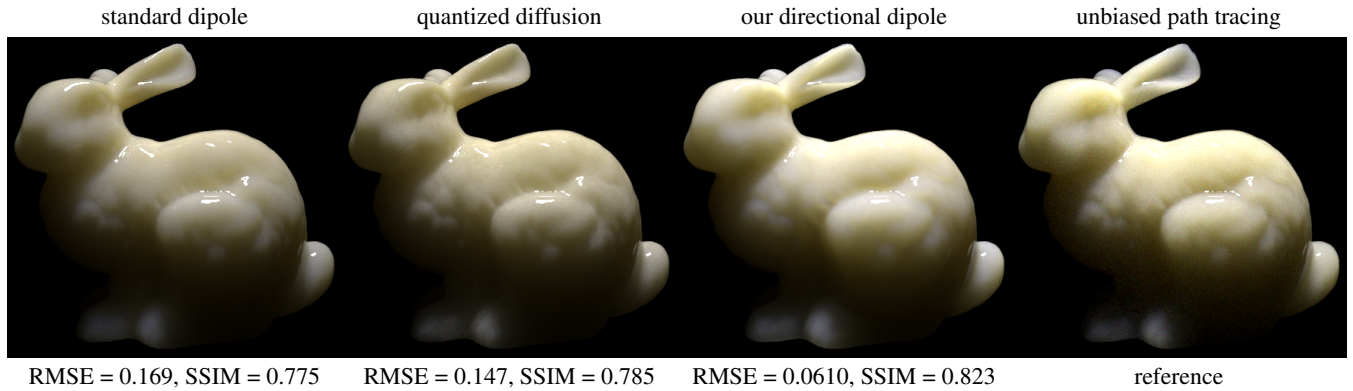


Fig. 1. Stanford bunny made of white grapefruit juice [Narasimhan et al. 2006]. It was rendered using different models for subsurface scattering. In the standard dipole [Jensen et al. 2001] and in quantized diffusion [d’Eon and Irving 2011], accurate single scattering was added using unbiased path tracing [Rushmeier 1988]. Our model captures translucency effects that are present in the full path tracing but not in the results of the other analytical BSSRDF models.

large. Hanrahan and Krueger [1993] pioneered efficient rendering of highly scattering translucent materials. They combined analytical single scattering in layers [Blinn 1982] with refractive boundaries and path traced multiple scattering. Stam [1995] introduced diffusion theory to evaluate multiple scattering using a finite element method. Dorsey et al. [1999] adapted a general Monte Carlo method called volume photon mapping [Jensen and Christensen 1998] for subsurface scattering. A fully analytical BSSRDF for subsurface scattering was first introduced to graphics by Jensen et al. [2001]. We refer to their model as the standard dipole in this paper. Our model is similar to the standard dipole in the sense that it is also fully analytic and does not use numerical approximation.

The standard dipole was combined with photon mapping by Donner and Jensen [2007]. They introduced an extended source model, which means that the standard dipole solution is integrated along the refracted ray. This method is referred to as photon diffusion. Although photon diffusion can take oblique incidence into account, the additional integration requires a larger number of samples than an analytical model such as the standard dipole or our model. D’Eon and Irving [2011] recently introduced an analytical extended source model. As in the standard dipole, they assume that light is normally incident. To solve the integral along the ray in the normal direction, they use a functional approximation based on a sum of Gaussians. In work concurrent with ours, Habel et al. [2013] showed that such integrals can be approximated efficiently using Monte Carlo integration instead of this functional approximation. Their algorithm is similar to photon diffusion and therefore takes oblique incidence into account. The key difference in our model is that we start from a fundamentally different solution of the diffusion equation for a ray of light in an infinite medium [Menon et al. 2005a; 2005b]. This solution enables us to derive the first analytical BSSRDF model which can take the directions of incident light rays into account. Unlike the other methods discussed here, our method does not require an expensive integration of the solution along the refracted ray.

Special case solutions for the diffusion equation are often derived for fluence (*scalar irradiance* in a volume) inside a medium with no boundary. It is however important to consider boundary conditions in computer graphics, where we are interested in the radiance emerging at the boundary. One popular approach to handle boundary conditions is the dipole approximation [Farrell et al. 1992; Jensen et al. 2001]. The dipole approximation was originally developed for handling light normally incident on a semi-infinite medium with a planar surface. We relax the assumption of normal incidence.

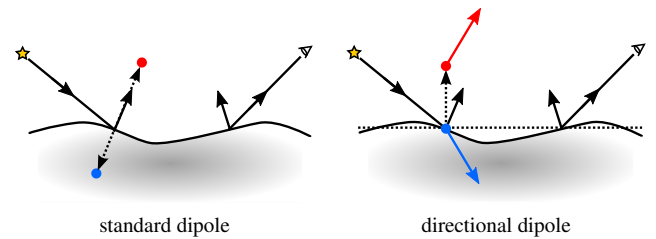


Fig. 2. A standard dipole model uses two point sources to handle boundary conditions. The points are displaced along the normal at the point of incidence. Our model uses two directional sources that are displaced along the normal of a plane containing the points of incidence and emergence.

The dipole model has been improved in a number of ways such as multipole [Wang 1998; Donner and Jensen 2005] and quadpole constructions [Kienle 2005; Donner and Jensen 2007]. Our model extends a directional source solution [Menon et al. 2005a; 2005b] to a dipole construction with a positive and a negative ray source (Figure 2). To the best of our knowledge, our work introduces a dipole extension with directional sources for the first time.

While our focus in this paper is to find an improved analytical model for subsurface scattering, another approach is to use pre-computation. Donner et al. [2009] introduced a method which pre-computes solutions to the radiative transfer equation as a canonical tabulated solution. Yan et al. [2012] proposed another pre-computation method for highly scattering media using a spherical Gaussian approximation. Both approaches relax the assumptions made in the models based on diffusion theory at the cost of storing precomputed tables. Unlike these methods, our model remains fully analytic. As such, the implementation of our model is trivial and incurs no extra memory cost or additional precomputation time.

### 3. THEORY

To have subsurface scattering in a surface rendering method, we use the general form of the rendering equation [Jensen et al. 2001]:

$$L_o(\mathbf{x}_o, \vec{\omega}_o) = L_e(\mathbf{x}_o, \vec{\omega}_o) + L_r(\mathbf{x}_o, \vec{\omega}_o) = L_e(\mathbf{x}_o, \vec{\omega}_o) + \int_A \int_{2\pi} S(\mathbf{x}_i, \vec{\omega}_i; \mathbf{x}_o, \vec{\omega}_o) L_i(\mathbf{x}_i, \vec{\omega}_i) (\vec{\omega}_i \cdot \vec{n}_i) d\omega_i dA, \quad (1)$$

where  $L_o(\mathbf{x}_o, \vec{\omega}_o)$  is the outgoing (or emergent) radiance in the direction  $\vec{\omega}_o$  from the location  $\mathbf{x}_o$  on the surface  $A$  of a medium,

$L_i(\mathbf{x}_i, \vec{\omega}_i)$  is the radiance incident on the surface  $A$  at the location  $\mathbf{x}_i$  from the direction  $\vec{\omega}_i$ , and  $\vec{n}_i$  is the surface normal at  $\mathbf{x}_i$ . The term  $L_e$  is the emitted radiance while  $L_r$  is the reflected radiance. The function  $S$  is a *Bidirectional Scattering-Surface Reflectance Distribution Function* (BSSRDF).

The BSSRDF is defined by the factor of proportionality between an element of emergent radiance  $dL_r(\mathbf{x}_o, \vec{\omega}_o)$  and an element of incident flux  $d\Phi_i(\mathbf{x}_i, \vec{\omega}_i)$  [Nicodemus et al. 1977]

$$S(\mathbf{x}_i, \vec{\omega}_i; \mathbf{x}_o, \vec{\omega}_o) = \frac{dL_r(\mathbf{x}_o, \vec{\omega}_o)}{d\Phi_i(\mathbf{x}_i, \vec{\omega}_i)}. \quad (2)$$

Typically, the BSSRDF is split into three terms: reduced intensity (direct transmission), single scattering, and multiple scattering [Hanrahan and Krueger 1993; Jensen et al. 2001]. Previous models for subsurface scattering focus on the definition of the multiple scattering term and leave the remaining terms to be computed separately using other methods (or the other way around [Hanrahan and Krueger 1993]). However, this separation is not always convenient. To date, there is seemingly no accurate and efficient method for rendering single scattering in translucent materials (that is, optically thick media with smooth, refractive boundaries). We are only aware of approximate methods for single scattering which assume a BSDF configuration [Blinn 1982; Hanrahan and Krueger 1993], approximate transmission distance [Jensen et al. 2001], non-refractive boundaries [Sun et al. 2005], an optically thin medium [Walter et al. 2009], or rough boundaries [Habel et al. 2013]. To get accurate single scattering, we have to rely on path tracing, which can be computationally expensive.

Instead of splitting the BSSRDF in three terms, we formulate our model such that it includes single scattering based on the delta-Eddington ( $\delta E$ ) approximation [Joseph et al. 1976]. In this approximation, the part of the single scattering that continues along the refracted ray is moved to the reduced intensity term  $S_{\delta E}$ . We then consider multiple scattering and the remaining single scattering to be the diffusive part of the BSSRDF  $S_d$ . The full BSSRDF in this approximation becomes

$$S = T_{12}(S_d + S_{\delta E})T_{21}, \quad (3)$$

where  $T_{12}$  and  $T_{21}$  are the Fresnel transmittance terms at the locations where the radiance enters and exits the medium, respectively.

The modified reduced intensity term  $S_{\delta E}$  is defined as the usual reduced intensity term but using a modified set of scattering properties [Joseph et al. 1976]:

$$\tilde{\sigma}_s = \sigma_s(1 - g^2), \quad \tilde{\sigma}_t = \tilde{\sigma}_s + \sigma_a, \quad \tilde{g} = g/(g + 1), \quad (4)$$

where  $\sigma_a$  is the absorption coefficient,  $\sigma_s$  is the scattering coefficient, and  $g$  is the asymmetry parameter (the mean cosine of the scattering angle). These  $\delta E$  scattering properties replace the corresponding scattering properties in the standard definition of the reduced intensity term. We return to the definition of this modified reduced intensity in Sections 3.1 and 3.2.

*Overview.* In the following, we describe how we derive  $S_d$ . The main idea is to consider both the origin and the direction of the refracted light ray within the medium. We can then use a solution to the diffusion equation where this ray is the source term. This solution gives us a formula for estimating the fluence at any point in the surrounding medium. Unlike existing models that use point sources, this formula is not only a function of distance, but also a function of the angle between the ray direction and the direction toward the position that we are interested in. Once this solution is established, we consider boundary conditions by introducing a

dipole with ray sources, and use the formula to find the radiance emerging from the medium at a point on the boundary. This leads to a new analytical BSSRDF which takes the direction of the incident light and the direction toward the point of emergence into account.

### 3.1 Diffusion Theory for a Ray of Light

As in previous work, we derive the diffusive part of the BSSRDF  $S_d$  using diffusion theory. This is usually done by finding a special case solution for the classic diffusion equation, which is [Ishimaru 1978]

$$(D\nabla^2 - \sigma_a)\phi_d(\mathbf{x}) = -q(\mathbf{x}) + 3D\nabla \cdot \mathbf{Q}(\mathbf{x}), \quad (5)$$

where  $\phi_d(\mathbf{x}) = \int_{4\pi} L_d(\mathbf{x}, \vec{\omega}') d\omega'$  is the diffusive part of the fluence,  $D$  is the diffusion coefficient, and  $q$  and  $\mathbf{Q}$  are zeroth and first order source terms.

The standard dipole model [Jensen et al. 2001] uses the solution of the diffusion equation for a point source in an infinite medium. Consequently, the diffusive part of this model depends only on the distance between the points of incidence and emergence. The direction of the incident light ray affects only the Fresnel transmittance term. Our key contribution is a new BSSRDF model based on a more recent solution to the diffusion equation for a ray of light in an infinite medium [Menon et al. 2005a; 2005b]. Our model thus takes the directions of incident light rays into account.

Consider a ray from the origin along the  $z$ -axis in a Cartesian  $xyz$  coordinate system. In the  $\delta E$  approximation, the reduced intensity (or directly transmitted) light due to this source is

$$L_{r1}(\mathbf{x}, \vec{\omega}) = \Phi\delta(x)\delta(y)\Theta(z)e^{-\tilde{\sigma}_t z}\delta(\vec{\omega} - \vec{\omega}_z), \quad (6)$$

where  $\Phi$  is the radiant flux of the source. We have set  $\mathbf{x} = (x, y, z)$  while  $\vec{\omega}_z$  is the direction of the  $z$ -axis and  $\Theta(z)$  is the Heaviside step function which is 1 when  $z \geq 0$  and 0 otherwise (it defines a half-line starting at the origin). This ray source leads to the following zeroth and first order source terms:

$$q(\mathbf{x}) = \tilde{\sigma}_s\Phi\delta(x)\delta(y)\Theta(z)e^{-\tilde{\sigma}_t z} \quad (7)$$

$$\mathbf{Q}(\mathbf{x}) = \tilde{g}q(\mathbf{x})\vec{\omega}_z, \quad (8)$$

These terms would be simpler if we were using an isotropic point source, especially the first order source term  $\mathbf{Q}(\mathbf{x})$ , which would then be zero. With Equation 8, we can more accurately represent the anisotropy of the radiance. The region around the origin where anisotropy is important grows with the asymmetry parameter  $g$  [Bevilacqua and Depeursinge 1999]. This anisotropy is not accurately represented by the extended source models [Donner and Jensen 2007; d'Eon and Irving 2011; Habel et al. 2013] since they rely on (an integration of) the isotropic point source solution.

As in the standard dipole, we assume that the point of estimation is not too close to sources and boundaries ( $|\mathbf{x}| \gg 1/\sigma_s$ ) and that the medium is a weak absorber ( $\sigma_a \ll \sigma_s$ ). Inserting the source terms (7–8) into the diffusion equation (5) and making these assumptions, we reach an approximate directional solution for a ray of light in an infinite medium [Menon et al. 2005a; 2005b]:

$$\phi'_d(r, \theta) = \frac{\Phi}{4\pi D} \frac{e^{-\sigma_{tr}r}}{r} \left( 1 + 3D \frac{1 + \sigma_{tr}r}{r} \cos\theta \right), \quad (9)$$

where  $\sigma_{tr} = \sqrt{\sigma_a/D}$  is the effective transport coefficient,  $r = |\mathbf{x}|$  is the distance from the point of incidence, and  $\theta$  is the angle with the ray direction (see Figure 3);

$$\cos\theta = z/r = (\mathbf{x} \cdot \vec{\omega}_z)/r. \quad (10)$$

It is interesting to note that, for a ray of light which is perpendicular to the direction toward the point of interest ( $\cos\theta = 0$ ),

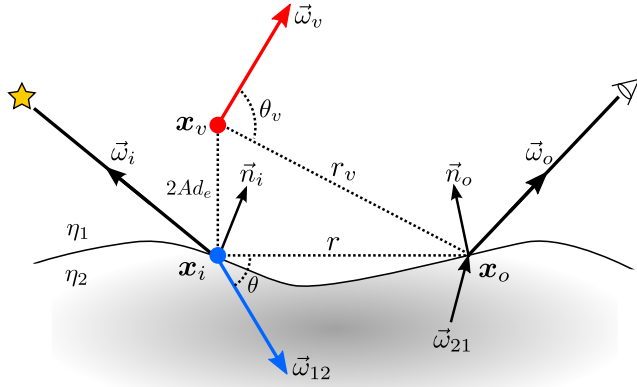


Fig. 3. Dipole configuration of our model. It is similar to the dipole with point sources, but we have ray sources. The direction  $\vec{\omega}_{12}$  of the refracted ray is used for the real source (blue). We mirror this direction in a modified tangent plane to find the direction  $\vec{\omega}_v$  of the virtual source (red). The modified tangent plane contains  $\mathbf{x}_o - \mathbf{x}_i$ , and it is perpendicular to the plane spanned by  $\vec{n}_i$  and  $\mathbf{x}_o - \mathbf{x}_i$ . The origin of the virtual source is displaced along the normal of this modified plane. Note that  $\theta \neq \theta_v$  and  $r \neq r_v$ .

Equation 9 turns into the point source solution which is used in existing analytical BSSRDF models [Jensen et al. 2001; d’Eon and Irving 2011]. We use a prime to indicate that a solution disregards boundaries ( $\phi'_d$  above and also  $S'_d$  in the following).

Suppose we have incident radiance  $L_i(\mathbf{x}_i, \vec{\omega}_i)$  and let it refract into a scattering material to get the transmitted radiance

$$L_t(\mathbf{x}_i, \vec{\omega}_{12}) = \eta^{-2} T_{12} L_i(\mathbf{x}_i, \vec{\omega}_i), \quad (11)$$

where  $\eta = \eta_2/\eta_1$  is the relative refractive index and  $\vec{\omega}_{12}$  is the direction of the refracted ray given by the law of refraction applied to  $\vec{\omega}_i$ . To use a refracted ray of arbitrary origin and direction as the ray source in our model, we have  $\mathbf{x} = \mathbf{x}_o - \mathbf{x}_i$  and the following setup for Equation 9 (see Figure 3):

$$\Phi = T_{12} \Phi_i, \quad \vec{\omega}_z = \vec{\omega}_{12}, \quad r = |\mathbf{x}|, \quad \cos \theta = \frac{\mathbf{x} \cdot \vec{\omega}_{12}}{r}.$$

### 3.2 Emergent Radiance

We now briefly return to the reduced intensity term and then describe how we obtain the emergent radiance from the fluence using approximations that were also used by d’Eon and Irving [2011].

Due to the delta-Eddington approximation, the transmitted radiance (11) and the radiance due to  $\delta E$  reduced intensity (6) enable us to indirectly define the modified reduced intensity part of the BSSRDF  $S_{\delta E}$ . The  $\delta E$  modified direct transmission emerging from the medium is

$$L_{r,\delta E}(\mathbf{x}_o, \vec{\omega}_o) = \eta^2 T_{21} e^{-\tilde{\sigma}_t s} L_t(\mathbf{x}_{ri}, \vec{\omega}_{21}), \quad (12)$$

where  $\mathbf{x}_{ri} = \mathbf{x}_o - s \vec{\omega}_{21}$  is the only point on the surface that can contribute to this reduced intensity term,  $s$  is the distance from  $\mathbf{x}_o$  to this point, and  $\vec{\omega}_{21}$  is the direction of the ray from inside the medium refracting to the direction  $\vec{\omega}_o$  according to the law of refraction. This term is easily evaluated using traditional ray tracing.

To get an expression for the diffusive part of the BSSRDF, we must relate the fluence to the emergent radiance. The emergent radiance  $L_{r,d}$  due to diffuse subsurface scattering is given by

$$L_{r,d}(\mathbf{x}_o, \vec{\omega}_o) = \eta^2 T_{21} L_d(\mathbf{x}_o, \vec{\omega}_{21}). \quad (13)$$

Combining the diffusion approximation [Ishimaru 1978] with Fick’s law of diffusion [Fick 1855], the diffusely scattered radiance is

$$L_d(\mathbf{x}, \vec{\omega}) = \frac{1}{4\pi} \phi_d(\mathbf{x}) - \frac{3}{4\pi} D \vec{\omega} \cdot \nabla \phi_d(\mathbf{x}) \quad (14)$$

with  $D = 1/(3\sigma'_t)$ , where  $\sigma'_t = \sigma_s(1-g) + \sigma_a$  is called the reduced extinction coefficient.

The relationship between  $L_d$  and the diffusive part of the BSSRDF  $S_d$  is given by Equations 2–3 and 13:

$$T_{12} S_d T_{21} = \eta^2 \frac{d(T_{21} L_d)}{d\Phi_i}. \quad (15)$$

Assuming that the diffusive light at the point of emergence no longer depends on the outgoing direction due to a large number of scattering events, we have  $S_d(\mathbf{x}_i, \vec{\omega}_i; \mathbf{x}_o, \vec{\omega}_o) = S_d(\mathbf{x}_i, \vec{\omega}_i; \mathbf{x}_o)$ . Integrating over outgoing directions, we get

$$T_{12} S_d(\mathbf{x}_i, \vec{\omega}_i; \mathbf{x}_o) 4\pi C_\phi(1/\eta) = \frac{dM_d(\mathbf{x}_o)}{d\Phi_i(\mathbf{x}_i, \vec{\omega}_i)}, \quad (16)$$

where  $M_d$  is the diffuse radiant exitance and  $C_\phi$  is a function of  $\eta$  which relates to hemispherical integration of the Fresnel transmittance (see Appendix A). The  $\eta^2$  factor cancels out because  $1/\eta$  was chosen as the argument of  $C_\phi$  [Aronson 1995]. The diffuse radiant exitance is

$$M_d(\mathbf{x}_o) = \int_{2\pi} T_{21} L_d(\mathbf{x}_o, \vec{\omega}_{21}) (\vec{n}_o \cdot \vec{\omega}_{21}) d\omega_o, \quad (17)$$

where  $\vec{n}_o$  is the surface normal pointing outward at the point of emergence such that the integral is over the hemisphere with  $\vec{n}_o \cdot \vec{\omega}_o > 0$ . Inserting the expression for  $L_d$  (14), we get an integral that has been investigated many times before [Haskell et al. 1994; Aronson 1995; Kienle and Patterson 1997]. The solution is

$$M_d(\mathbf{x}_o) = C_\phi(\eta) \phi_d(\mathbf{x}_o) - C_E(\eta) D \vec{n}_o \cdot \nabla \phi_d(\mathbf{x}_o), \quad (18)$$

where  $C_\phi$  and  $C_E$  are in Appendix A. Equation 18 was also used in the BSSRDF model of d’Eon and Irving [2011].

As opposed to previous work, we now use the diffuse fluence from the directional solution (9). The gradient of this expression is

$$\nabla \phi'_d = \frac{\Phi}{4\pi D} \frac{e^{-\sigma_{tr} r}}{r^3} \left( \vec{\omega}_{12} 3D(1 + \sigma_{tr} r) - \mathbf{x} (1 + \sigma_{tr} r) - \mathbf{x} 3D \frac{3(1 + \sigma_{tr} r) + (\sigma_{tr} r)^2}{r} \cos \theta \right). \quad (19)$$

Inserting the directional solution (9) and its gradient (19) into Equation 18, we get an expression for the diffuse radiant exitance  $M_d$ . When this is inserted in Equation 16, we obtain an expression for the diffusive part of the BSSRDF when disregarding boundaries:

$$S'_d(\mathbf{x}, \vec{\omega}_{12}, r) = \frac{1}{4C_\phi(1/\eta)} \frac{1}{4\pi^2} \frac{e^{-\sigma_{tr} r}}{r^3} \left[ C_\phi(\eta) \left( \frac{r^2}{D} + 3(1 + \sigma_{tr} r) \mathbf{x} \cdot \vec{\omega}_{12} \right) - C_E(\eta) \left( 3D(1 + \sigma_{tr} r) \vec{\omega}_{12} \cdot \vec{n}_o - \left( (1 + \sigma_{tr} r) + 3D \frac{3(1 + \sigma_{tr} r) + (\sigma_{tr} r)^2}{r^2} \mathbf{x} \cdot \vec{\omega}_{12} \right) \mathbf{x} \cdot \vec{n}_o \right) \right], \quad (20)$$

where  $T_{12}$  and the flux  $\Phi$  cancel out since  $\Phi = T_{12} \Phi_i$ , and we take the derivative with respect to  $\Phi_i$ . The factor  $(4C_\phi(1/\eta))^{-1}$  is the normalization factor also used by d’Eon and Irving [2011].

### 3.3 Boundary Conditions

The BSSRDF derived above (20) disregards boundaries in the sense that it was derived for a ray of light in an *infinite medium*. Since our purpose is to render media with boundaries, we need to take boundary conditions into account. Like existing BSSRDF models [Jensen et al. 2001; d'Eon and Irving 2011], we assume a semi-infinite medium with a flat boundary and apply the resulting model to arbitrary boundary conditions.

We note that any approximate boundary conditions, including ours and the ones that are used for existing models, are more or less empirically based. It is widely acknowledged [Aronson 1995, for example] that comparison with full solutions of the radiative transfer equation is the only reasonable way to evaluate the appropriateness of approximate boundary conditions. In the following, we provide reasoning behind each of our choices but only as motivation. We validate our final model via numerical experiments in Section 5.

**3.3.1 Dipole configuration.** There are many sensible ways to incorporate the boundary in diffusion theory, and one has to make a number of decisions when building a new model [Haskell et al. 1994]. One common approach is to let the fluence vanish at the boundary of the medium. This is achieved by introducing a virtual source which is the real source mirrored in the surface tangent plane; a configuration commonly referred to as a *dipole*. Unlike the standard dipole [Jensen et al. 2001], we have a dipole of ray sources. This influences how the sources should be positioned in the dipole. Figure 3 illustrates the configuration we have chosen.

The diffusion approximation matches the exact solution better if the fluence vanishes at an *extrapolated boundary*, that is, a boundary which is the same as the actual boundary but displaced outward in the normal direction [Glasstone and Edlund 1952; Davison 1958; Haskell et al. 1994; Aronson 1995]. The orthogonal distance from the actual boundary to this extrapolated boundary is called the extrapolation distance  $d_e$ . Existing models use  $d_e = 2D$ . This standard approximation for  $d_e$  was originally derived from diffusion theory for non-absorbing media with non-refractive boundaries ( $\eta = 1$ ). Comparing with exact calculations of  $d_e$  for this and other types of media, Aronson [1995] found that  $2D$  is imprecise in all cases. We thus use an approximation which is closer to the right  $d_e$  for weakly absorbing media with non-refractive boundary [Davison 1958]

$$d_e = 2.131 D / \sqrt{\alpha'} , \quad (21)$$

where  $\alpha' = \sigma'_s / \sigma'_t$  is the reduced scattering albedo which is the ratio of the reduced scattering coefficient  $\sigma'_s = \sigma_s(1 - g)$  to the reduced extinction coefficient  $\sigma'_t = \sigma'_s + \sigma_a$ .

If the boundary of the medium has a mismatch of refractive indices ( $\eta_1$  and  $\eta_2$ , see Figure 3), we must multiply the extrapolation distance by a reflection parameter  $A$  [Groenhuis et al. 1983]. When the real source is mirrored in the extrapolated boundary, the displacement of the virtual source becomes  $2Ad_e$ . The reflection parameter  $A$  is related to hemispherical integrals over the Fresnel transmittance [Aronson 1995]. We use the same reflection parameter as d'Eon and Irving [2011]. A convenient way to express  $A$  is

$$A(\eta) = \frac{1 - C_E(\eta)}{2C_\phi(\eta)} . \quad (22)$$

**3.3.2 Modified tangent plane.** Since our source is directional, we also need to mirror the direction as well as the origin. While one obvious choice of mirroring plane is the tangent plane, which is defined by  $\vec{n}_i$ , we found that this choice leads to an inaccurate solution if the assumption of a flat boundary is violated (which in practice is almost always the case). Instead, we mirror the source

using a modified tangent plane with normal

$$\vec{n}_i^* = \begin{cases} \vec{n}_i & , \text{ for } \mathbf{x}_o = \mathbf{x}_i \\ \frac{\mathbf{x}_o - \mathbf{x}_i}{|\mathbf{x}_o - \mathbf{x}_i|} \times \frac{\vec{n}_i \times (\mathbf{x}_o - \mathbf{x}_i)}{|\vec{n}_i \times (\mathbf{x}_o - \mathbf{x}_i)|} & , \text{ otherwise } \end{cases} . \quad (23)$$

As we will demonstrate in Section 6.2, this choice in particular eliminates issues in backlit regions. These issues are due to exaggerated directional effects caused by the assumption of a semi-infinite medium. The modification basically ensures that  $\cos \theta$  only changes in the virtual source as if the geometry were planar. Note that the modified normal is used only to set the position and the direction of the virtual source. The normal used for Fresnel and cosine terms is not affected. If the boundary is actually flat, or, more generally, if the point of emergence lies in the tangent plane defined by  $\vec{n}_i$ , the modified normal equals the normal at the point of incidence.

**3.3.3 Distance to the real source.** In the standard dipole, the real source is placed at the average depth  $z_r = 1/\sigma'_t = 3D$  of the first scattering event straight below the surface ( $1/\sigma'_t$  is often referred to as one transport mean free path). This is a first order approximation of the multipole which captures scattering due to a normally incident light ray [Eason et al. 1978]. This displacement of the real source leads to a modified distance to the real source  $d_r = \sqrt{r^2 + z_r^2}$  which is based on the assumption that the ray is normally incident on a planar surface [Jensen et al. 2001].

Since our source resembles the actual light ray more than it resembles the first scattering event, we do not displace the real source. This choice introduces a singularity in the model for  $r = 0$  (Equation 9 is valid only for  $r \gg 1/\sigma_s$ ). It also leads to overestimation in the region close to the singularity where the assumption of uniform emergent radiance is invalid. In Appendix B, we explain how to deal with this singularity by comparing our solution to similar solutions based on exact transport theory. Although the theoretical reasoning might be complicated, the final solution is quite simple. We correct the distance to the real source using

$$d_r^2 = \begin{cases} r^2 + D\mu_0(D\mu_0 - 2d_e \cos \beta) & , \text{ for } \mu_0 > 0 \text{ (frontlit)} \\ r^2 + 1/(3\sigma_t)^2 & , \text{ otherwise (backlit)} \end{cases} , \quad (24)$$

where  $\sigma_t = \sigma_a + \sigma_s$ ,  $\mu_0 = -\vec{n}_o \cdot \vec{\omega}_{12}$ , and the other cosine term is

$$\cos \beta = -\sin \theta \frac{r}{\sqrt{r^2 + d_e^2}} = -\sqrt{\frac{r^2 - (\mathbf{x} \cdot \vec{\omega}_{12})^2}{r^2 + d_e^2}} . \quad (25)$$

When introducing a distance correction, we must consider whether the denominator of  $\cos \theta$  (appearing in Equations 9 and 19) should be affected by the correction or not. Based on numerical experiments, we have found that correction of the denominator leads to smaller error. We therefore do not explicitly write  $\cos \theta$  in the  $S'_d$  function (20), as the denominator is then corrected by simply using  $d_r$  as the  $r$  argument of  $S'_d$  for the real source.

**3.3.4 Our BSSRDF.** Putting it all together, the diffusive part of our BSSRDF is

$$S_d(\mathbf{x}_i, \vec{\omega}_i; \mathbf{x}_o) = S'_d(\mathbf{x}_o - \mathbf{x}_i, \vec{\omega}_{12}, d_r) - S'_d(\mathbf{x}_o - \mathbf{x}_v, \vec{\omega}_v, d_v) , \quad (26)$$

where  $\mathbf{x}_v = \mathbf{x}_i + 2Ad_e\vec{n}_i^*$ ,  $d_v = |\mathbf{x}_o - \mathbf{x}_v|$ , and  $\vec{\omega}_v = \vec{\omega}_{12} - 2(\vec{\omega}_{12} \cdot \vec{n}_i^*)\vec{n}_i^*$  (see Figure 3). To obtain the full BSSRDF, we add the modified reduced intensity term  $S_{\delta E}$  and multiply by the Fresnel transmittances  $T_{12}$  and  $T_{21}$  (Equation 3).

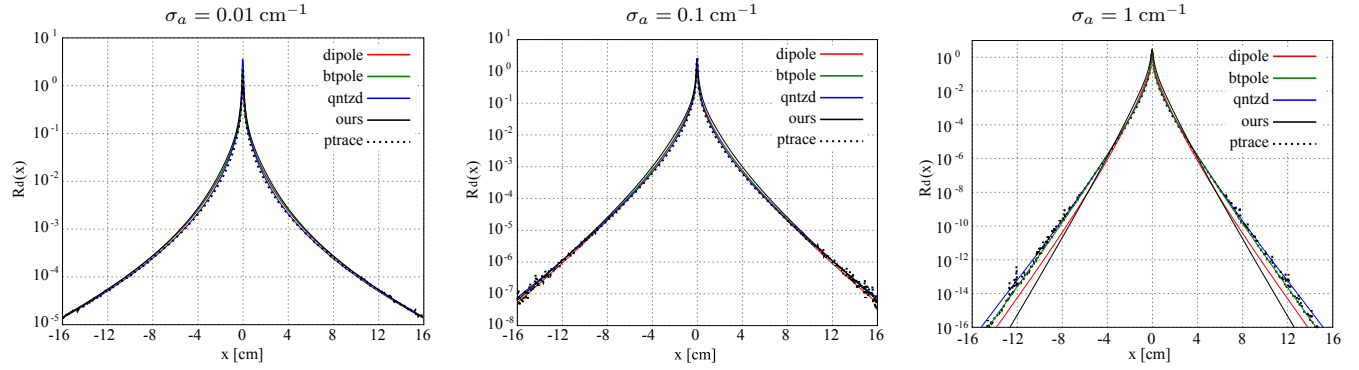


Fig. 4. Diffuse reflectance curves for a ray normally incident on planar, non-refractive semi-infinite media with  $\sigma_s = 1 \text{ cm}^{-1}$  but with different absorption properties ( $\sigma_a$  is specified above each plot). The ray is incident at the origin. The graphs plot diffuse reflectance  $R_d$  at positions along the  $x$ -axis for different models (identified in the legends using the abbreviations specified in Figure 7). Note that each vertical axis uses a log-scale with a different range.

#### 4. IMPLEMENTATION

Just like other BSSRDFs, our model can be used in a number of rendering approaches. The only major difference is that our model takes directions into account. Approaches which assume irradiance as input need relatively minor modification in order to use our model. We implemented our model in the following two approaches.

*Direct Monte Carlo integration.* As described by Jensen et al. [2001], it is possible to use a BSSRDF in a Monte Carlo ray tracer. We integrate the BSSRDF in a progressive path tracer by distributing points evenly across the surface of the translucent object using a dart throwing technique. A new set of points is sampled iteratively, and, for every sampled surface point, the incident illumination is sampled from one direction. When a ray hits a translucent material, we loop over all surface samples and accept or reject them using a Russian roulette with the exponential term in the BSSRDF,  $\exp(-\sigma_{tr}r)$ , as the probability of acceptance.

*Hierarchical integration.* The hierarchical integration method for the standard dipole model [Jensen and Buhler 2002] works well with our model. Our implementation is almost the same as the original method. The only difference is that the irradiance computation is no longer separable from the evaluation of the BSSRDF. Each irradiance sample will be a list of differential irradiance samples instead of its sum at the same location. We also use the same set of directions across all irradiance samples in order to spatially cluster them without any change in the original algorithm. Each evaluation of the BSSRDF now goes over the list and takes directions into account. The number of evaluations of the BSSRDF increases with this approach. One possible optimization would be to extend clustering to take into account directions, so that we can also cluster samples across directions. We chose a simpler approach of utilizing the existing implementation of the hierarchical integration method. In the results we present, we used 16 directional samples by importance sampling the environment map.

#### 5. RESULTS

We implemented the standard dipole [Jensen et al. 2001], quantized diffusion [d'Eon and Irving 2011], the better dipole [d'Eon 2012], and our model all with the two approaches mentioned in Section 4. The results in Figures 1, 7, and 8 were rendered using direct Monte Carlo integration. The results in Figure 11 were rendered using hierarchical integration. Optical properties measured by Jensen et

al. [2001] and Narasimhan et al. [2006] were used as input parameters. To validate our model, we compare with full solutions of the radiative transfer equation using unbiased path tracing [Rushmeier 1988]. Single scattering is computed using the same unbiased path tracing approach, and it is added to all the results of the existing models but not to the results of our model.

One common approach to compare BSSRDFs is to plot spatially resolved diffuse reflectance  $R_d$  for a ray which is normally incident on a planar semi-infinite medium. In this case,  $\mathbf{x}_i$  and  $\vec{\omega}_i$  are fixed so that we have

$$R_d(\mathbf{x}_o) = \int_{2\pi} S(\mathbf{x}_i, \vec{\omega}_i; \mathbf{x}_o, \vec{\omega}_o) (\vec{\omega}_o \cdot \vec{n}_o) d\omega_o. \quad (27)$$

Considering a non-refractive medium with its surface in the  $xy$ -plane and a BSSRDF which does not depend on  $\vec{\omega}_o$ , we have  $R_d(x, y) = \pi S_d(x, y)$ . Figure 4 shows diffuse reflectance curves for media with different albedos as produced by all the models we tested. We fixed  $\sigma_s = 1 \text{ cm}^{-1}$  and tested  $\sigma_a = 0.01 \text{ cm}^{-1}$ ,  $0.1 \text{ cm}^{-1}$ ,  $1 \text{ cm}^{-1}$  with  $\eta_1 = \eta_2 = 1$  and  $g = 0$ . Our model produces curves that are similar to existing models with slight overestimation. If we take the curves of quantized diffusion and add approximate diffuse single scattering [Habel et al. 2013] instead of path traced single scattering, we get curves which are very close to ours. This suggests that the overestimation in our model is due to approximation in single scattering. Note that the deviation of our model in the tail of the curve for highly absorbing media ( $\sigma_a = 1 \text{ cm}^{-1}$ ) is in fact very small in its scale. Moreover, as we demonstrate in our other results, the slight deviations in these diffuse reflectance curves are not as significant as the missing directional effects.

To demonstrate the missing directional effects, we also compare diffuse reflectance curves for oblique incidence. Figure 5 uses the same configuration as Figure 4, except that we now change the angle of incidence away from  $0^\circ$ . The  $x$ -axis is in the plane of incidence. We tested the medium with  $\sigma_a = 0.01 \text{ cm}^{-1}$ , and we included the other models to verify that single scattering has minor directional effects. In these plots, only our model captures the characteristic distortion of the curve according to the angle of incidence, especially at  $60^\circ$ . Figure 6 visualizes the region around the peak as 2D plots over the surface of the medium. The curves in Figure 5 correspond to horizontal slices through the middle of the plots in Figure 6. In the 2D plots, we compare our model with quantized diffusion plus path traced single scattering and with unbiased path tracing. While both analytical models do not perfectly match the path traced reference,

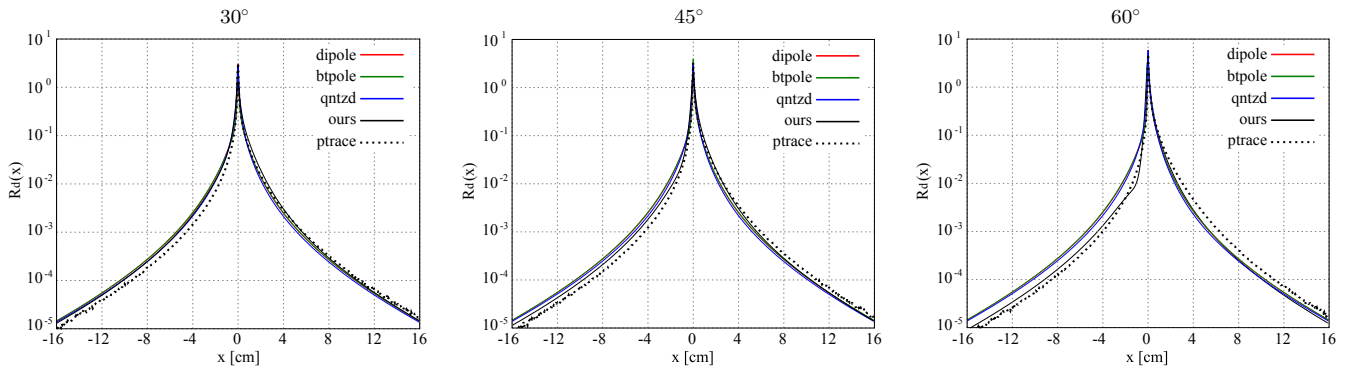


Fig. 5. Diffuse reflectance curves for a ray obliquely incident on a planar, non-refractive semi-infinite medium. The ray is incident at the origin at different angles with the normal (the angles are specified above each plot), and the  $x$ -axis is in the plane of incidence. Curves are plotted for the same models as in Figure 4. We used  $\sigma_s = 1 \text{ cm}^{-1}$  and  $\sigma_a = 0.01 \text{ cm}^{-1}$ .

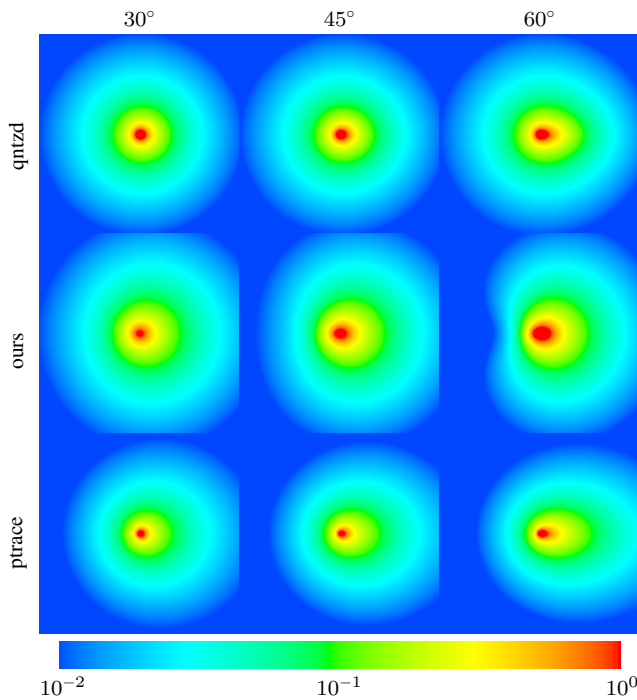


Fig. 6. False-color images visualizing  $R_d(x, y)$  in the region  $[-2 \text{ cm}, 2 \text{ cm}] \times [-2 \text{ cm}, 2 \text{ cm}]$ . These 2D slices have the same configuration as the plots in Figure 5. The first row is quantized diffusion plus path traced single scattering (qntzd), the second row is our directional dipole (ours), and the third row is unbiased path tracing (ptrace). The angles of incidence are at the top. We used  $\sigma_s = 1 \text{ cm}^{-1}$  and  $\sigma_a = 0.01 \text{ cm}^{-1}$ . Our model varies significantly with the angle of incidence, while quantized diffusion varies only due to single scattering.

our model distorts the reflectance according to the angle of incidence as in the reference, especially along the  $x$ -axis (parallel to the plane of incidence). The quantized diffusion slices exhibit only very slight variations which are all due to the added single scattering.

Although diffuse reflectance plots for semi-infinite media can be informative, what is more important in practice is the accuracy of rendered images in more complex cases with refractive boundaries that are not flat. Figure 7 compares rendered images of simple shapes

with different materials. Figure 9 plots the root-mean-squared error (RMSE) and the structural similarity index (SSIM [Wang et al. 2004]) of the corresponding high dynamic range images (using perceptually uniform encoding for SSIM [Aydın et al. 2008]). Our model produces results that are significantly closer to path traced references when the material is highly forward scattering. For such cases, directionality of incident light is important since light generally maintains its initial direction over longer distances. This makes the directional effects non-negligible in the resulting radiance distribution. For isotropically scattering materials (first four materials), existing models are comparable to our model. We however note that this is true only if accurate path traced single scattering is added to the existing models (Figure 9, full color). The error nearly doubles if single scattering is not added (Figure 9, faded color).

Figure 1 shows the bunny model rendered with the white grapefruit juice material as an example of more complex geometries. The result of our model is again closer to the path traced reference. In particular, our model captures bright scattered highlights which are missing in existing models. Figure 8 shows the same scene configuration with the marble material. For this material, existing models tend to work well, yet our model is still more accurate than the other models. The squared differences between BSSRDF results and the path traced references in Figures 1 and 8 are visualized in Figure 10. Figure 11 demonstrates renderings with image-based lighting using hierarchical integration. Our model captures details of the geometry that are highlighted by the directionality of the incident illumination. These details are lost with the existing models.

It is noteworthy that a model which has fairly accurate diffuse reflectance curves does not necessarily produce accurate rendered images. Although our model has normal incidence curves which are slightly less accurate (Figure 4), the rendered images are generally more accurate than if we use the existing models. This discrepancy is due to the fact that the existing models do not consider the direction toward the point of emergence (Figure 6) nor does diffuse reflectance curves capture it (Figure 5), and also that fundamental assumptions such as semi-infinite media are not valid in practice.

In direct Monte Carlo integration, there is little practical difference in using our model instead of the standard (or better) dipole. For each evaluation of the BSSRDF, we simply replace a single scattering evaluation by a few additional arithmetic operations in the diffusive part. It is significantly faster to evaluate our BSSRDF than to evaluate the quantized diffusion BSSRDF. In order to make the evaluation costs of quantized diffusion of the same order of magni-

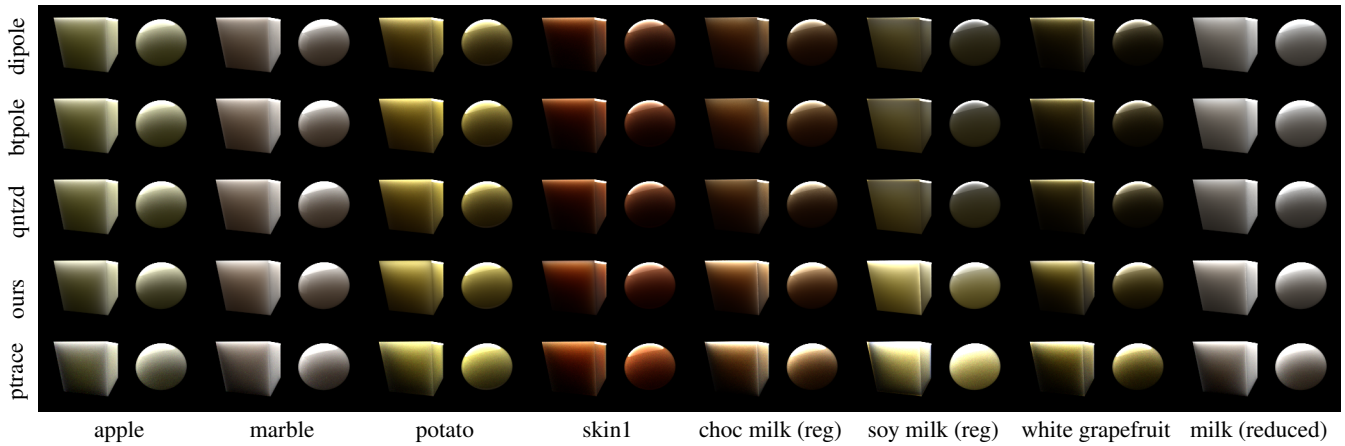


Fig. 7. Simple test cases comparing the standard dipole model (dipole) [Jensen et al. 2001], the better dipole model (btpole) [d’Eon 2012], quantized diffusion (qntzd) [d’Eon and Irving 2011], our model (ours), and the reference solutions rendered by path tracing (ptrace). Path traced single scattering was added to the existing models but not to ours. Materials used are all from measured values [Jensen et al. 2001; Narasimhan et al. 2006]. The results of our model are closer to the path traced references or equally good, while the rendering times are shorter as our model includes single scattering.

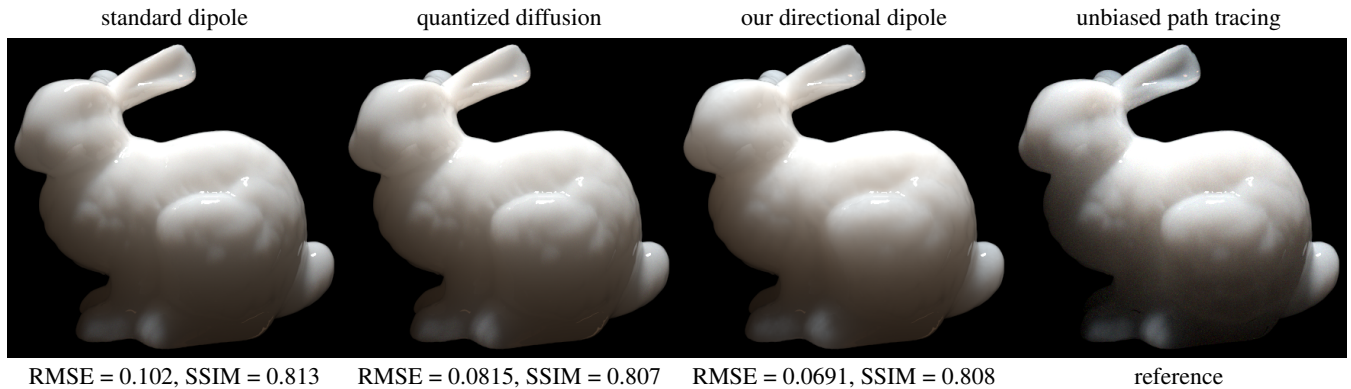


Fig. 8. Same scene configuration as Figure 1 but with marble [Jensen et al. 2001]. Although existing models work rather well for this material, our model is still closer to the path traced reference solution in terms of error. Perceptually, our result seems too smooth. This is due to the assumption that emerging light is diffuse. The same assumption is used in the other analytical models, but, for those models, the problem is partly mitigated by the path traced single scattering.

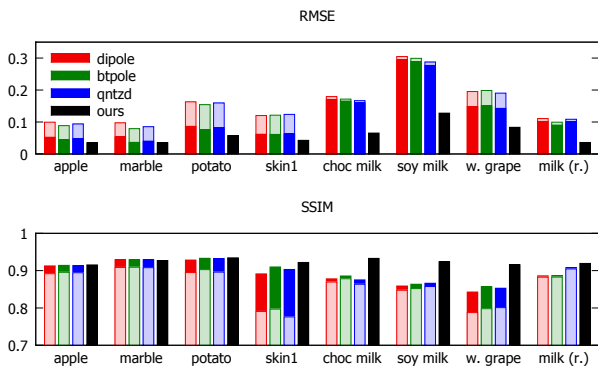


Fig. 9. Objective image quality measurements for the renderings in Figure 7. Every measurement for an existing model (full color) is accompanied by a measurement where path traced single scattering is excluded (faded color). Our model outperforms the other models, except if materials have high albedo and scatter isotropically, then the other models can be equally good when single scattering is added.

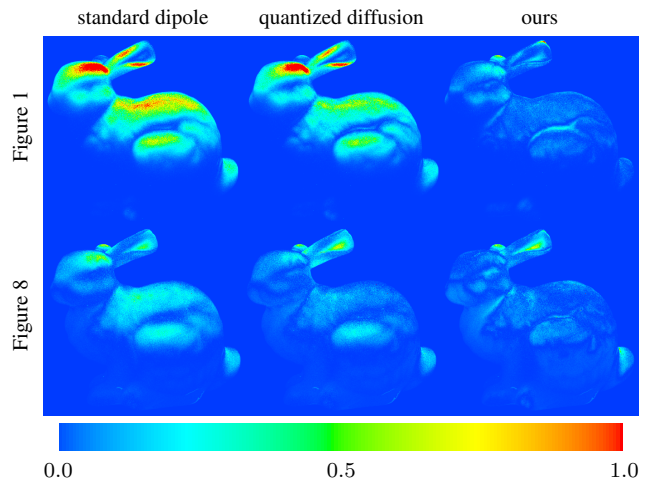


Fig. 10. Squared differences of BSSRDF results versus references.





Fig. 11. Image based lighting of the Happy Buddha model with the materials also used in the simple test cases (Figure 7). The images were rendered using hierarchical integration of the quantized diffusion model [d’Eon and Irving 2011] plus single scattering added by separate Monte Carlo ray tracing (top row) and our model (bottom row). We excluded Fresnel reflection in order to better highlight the differences between the two models.

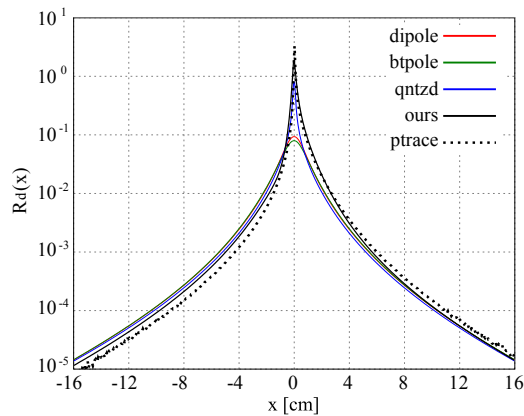


Fig. 12. Diffuse reflectance curves for a ray incident at a  $45^\circ$  angle without adding path traced single scattering to the existing models. Both the standard dipole and the better dipole now miss a sharp peak around the origin. While the quantized diffusion model maintains the sharp peak, there is no characteristic shifting of the profile due to the oblique angle of incidence.

tude as the other models, we needed to implement the radial caching technique of d’Eon and Irving [2011]. This technique cannot be used in the same way with our model due to the dependency on directions. Similarly, in our current implementation of hierarchical integration, we must (as opposed to existing models) evaluate the diffusive part of our BSSRDF for every direction of incident illumination that we consider. On the other hand, the single scattering which is added separately to the existing models also depends on directions, and its cost is thus also proportional to the number of directional samples. Usually, the number of directional samples must be very large to obtain noiseless single scattering.

In terms of rendering time, full unbiased path tracing in common scenes with a refractive medium and a small light source (Figures 1 and 8) takes days using one CPU. Excluding multiple scattering in our path traced results was only a factor of four or less faster. In a scene with a large light source (Figures 7 and 11), path tracing is up to two orders of magnitude faster, but still takes several hundred seconds. It is thus very expensive to add single scattering in the existing models, where it can easily take up 90% of the total rendering time. One option to reduce the computational costs of single scattering is to use some approximation, as suggested in previous work [Hanrahan and Krueger 1993; Jensen et al. 2001; Habel et al. 2013]. Such approximation however introduces further error in the rendered images. This makes our model even more favorable in terms of accuracy. Figure 12 shows the consequences in the diffuse reflectance curves if we exclude single scattering.

In most cases, path traced single scattering makes the total rendering time of existing models larger than if our model is used. However, this is not the case in Figure 11, as we used hierarchical integration and the light source is large (due to the environment map we used). The images in the bottom row of Figure 11, which were rendered with our model using 16 directions and 4 samples per pixel, took 18–20 minutes each on a 3.4 GHz CPU (Intel Core i7-2600) using a single thread. As a representative of the existing models, quantized diffusion with radial caching and with added single scattering produced each of the images in the top row of Figure 11 in 13–14 minutes. Thus, in this unfavorable case of Figure 11, our model is a factor 1.4 more expensive than the existing models.

## 6. DISCUSSION

### 6.1 Negative values

In some cases, our model can return a negative value. Figure 13 illustrates such cases with the index-matched boundary. We have found

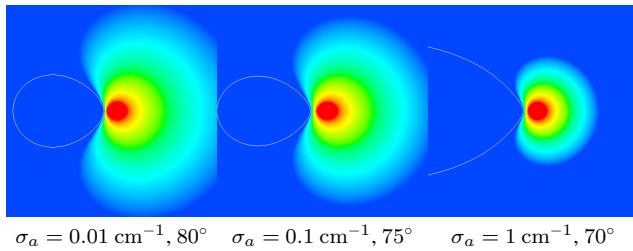


Fig. 13. Negative values appear in our model at grazing incidence. These 2D slices are similar to those in Figure 6, but with different absorption coefficients and angles of incidence (the values are specified at the bottom). The regions enclosed by a white contour have been clamped to zero. For highly absorbing media, our model can return negative values for even smaller angles. No configuration in Figure 6 has such a clamped region.

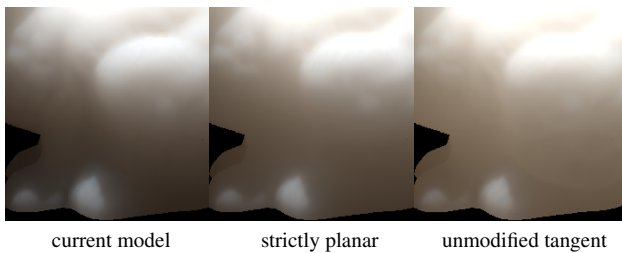


Fig. 14. Comparison of our current model, our model if we assume a strictly planar boundary instead of the modified tangent plane. The images are close ups of the bunny in Figure 8 without Fresnel reflections to highlight the differences. The strictly planar variant is close to the current model, but misses subtle details and slightly overestimates. The use of the modified tangent plane is important for our model to work well.

that our model tends to return a negative value when the albedo is low and the angle of incidence is large. It is mainly a consequence of the approximations in the ray source solution (Equation 9). Our current solution is to simply clamp the final value to zero if it is negative. We have not found a case where clamping causes visible artifacts. We also note that negative values rarely occur if a medium has an index of refraction larger than the surrounding medium as is commonly the case.

## 6.2 Strictly planar model and modified tangent plane

Since our boundary conditions are approximative, as in the existing models, it is possible to consider some other theoretically reasonable variations of the final model in Equation 26. For example, while our model uses distances and angles computed directly from given locations and directions, we could assume a strictly planar configuration (with  $\vec{n}_o$  always perpendicular to  $\mathbf{x}$  in Equation 20) and compute distances and angles accordingly. This approach is used in existing analytical models [Jensen et al. 2001; d’Eon and Irving 2011; d’Eon 2012]. As explained before, we could also mirror sources according to the normal at the point of incidence ( $\vec{n}_i$ ) instead of the normal of the modified tangent plane ( $\vec{n}_i^*$ ).

Figure 14 compares such potential variants of our model. This comparison demonstrates that, if we assume a strictly planar boundary as in the existing models, we would slightly blur illumination features that are present with our current model. Moreover, we have found that the strictly planar variant as well as the variant without the modified tangent plane usually overestimate illumination in backlit

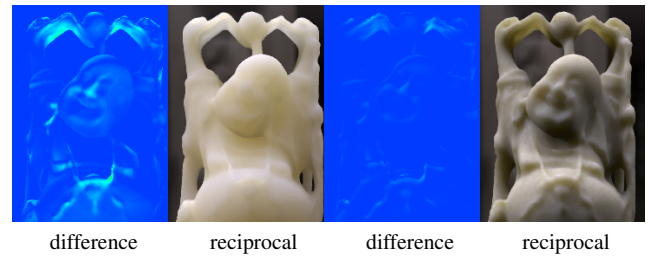


Fig. 15. Taking the average of two evaluations of our model with the variables of incoming and outgoing light swapped around would make our model reciprocal. The difference from the non-reciprocal image in Figure 11 depends on the material.

regions. Although this result does not conclude that our choices are fundamentally better than other variants, we have found that it is rather difficult to improve upon the final model so that accuracy is improved across all our test cases.

## 6.3 Reciprocity

Unlike the standard dipole model and the quantized diffusion model, both of which only depend on the distance, our model is not reciprocal. In other words, swapping variables for a point of incidence and a point of emergence does not result in the same value in our model. If a reciprocal model is desirable (e.g., for bidirectional rendering algorithms), one can take the average of two evaluations of our model with swapped variables. Figure 15 shows images rendered with this modification. For highly scattering materials (right), we have found that our model is close to reciprocal, meaning that this modification would not result in significant changes in rendered images. For thinner media (left), however, this modification produces some differences in rendered images. We have not fully investigated whether these differences are generally desirable or not in terms of accuracy. All other results in this paper do not use this modification.

## 6.4 Limitations

Since we still make a number of assumptions to derive our model, it does not perfectly match the results of path tracing. This is evident in Figure 6, for example. Our model also does not reproduce emergent radiance distributions that are not uniform. In addition, our model does not distinguish between materials with different scattering coefficients ( $\sigma_s$ ) and asymmetry parameters ( $g$ ) if they result in the same reduced scattering coefficient ( $\sigma'_s = \sigma_s(1 - g)$ ), except in the correction of the distance to the real source (Section 3.3.3).

We emphasize again that, similar to other models, our model is derived under the assumption of a planar semi-infinite medium. The modified tangent plane does not remove this limitation. This assumption is known to have issues in a number of cases such as sharp boundaries and thin features. Extensions of our model to quadpole and multipole constructions to alleviate those issues are interesting future work.

## 7. CONCLUSION

We introduced a novel BSSRDF which comes closer to path traced references than existing models. Our model is built upon a new analytical solution to the diffusion equation which enables us to take the direction of incoming light into account. We explained how to derive a practical BSSRDF by extending this solution into a dipole of real and virtual ray sources. Our work significantly improves the accuracy of an analytical model based on diffusion

theory. Improvement over existing models is especially significant for highly forward scattering materials, where the directionality of the incident illumination is more important. We believe that our model is a valuable addition to the existing set of analytical BSSRDFs. Since our model is fully analytic, application to real-time rendering is very promising as compared with models based on numerical integration.

#### ACKNOWLEDGMENTS

We would like to thank Jesper Mosegaard for funding through the Digital Prototypes project. We would also like to thank Eugene d'Eon for helping us with the quantized diffusion model.

#### APPENDIX

##### A. FRESNEL INTEGRALS

In Section 3.2, we need hemispherical integrals of the Fresnel transmittance  $T$ . More specifically, we need to evaluate the cosine-weighted hemispherical integral of  $T_{21}$  multiplied by the  $L_d$  in Equation 14. To do this, we use the following functions

$$C_\phi(\eta) = \frac{1}{4\pi} \int_{2\pi} T_{21}(\eta, \theta_o) \cos \theta_o d\omega \quad (28)$$

$$C_E(\eta) = \frac{3}{4\pi} \int_{2\pi} T_{21}(\eta, \theta_o) \cos^2 \theta_o d\omega, \quad (29)$$

where  $\cos \theta_o = \vec{n}_o \cdot \vec{\omega}_o$ . In the following, we leave out the argument of the  $C$ -functions to shorten notation. The  $C$ -functions are easily written in terms of Fresnel reflectance  $R$  instead of Fresnel transmittance, since  $T = 1 - R$ . This means that

$$C_\phi = \frac{1}{4\pi} \left( \pi - \int_{2\pi} R_{21}(\eta, \theta_o) \cos \theta_o d\omega \right) = \frac{1}{4} (1 - 2C_1) \quad (30)$$

$$C_E = \frac{3}{4\pi} \left( \frac{2\pi}{3} - \int_{2\pi} R_{21}(\eta, \theta_o) \cos \theta_o d\omega \right) = \frac{1}{2} (1 - 3C_2). \quad (31)$$

D'Eon and Irving [2011] also use the functions  $C_\phi$  and  $C_E$ , and they provide the following convenient polynomial approximations to ease their evaluation:

$$2C_1 \approx \begin{cases} 0.919317 - 3.4793\eta + 6.75335\eta^2 - 7.80989\eta^3 \\ \quad + 4.98554\eta^4 - 1.36881\eta^5, & \eta < 1 \\ -9.23372 + 22.2272\eta - 20.9292\eta^2 + 10.2291\eta^3 \\ \quad - 2.54396\eta^4 + 0.254913\eta^5, & \eta \geq 1 \end{cases}$$

$$3C_2 \approx \begin{cases} 0.828421 - 2.62051\eta + 3.36231\eta^2 - 1.95284\eta^3 \\ \quad + 0.236494\eta^4 + 0.145787\eta^5, & \eta < 1 \\ -1641.1 + \frac{135.926}{\eta^3} - \frac{656.175}{\eta^2} + \frac{1376.53}{\eta} + 1213.67\eta \\ \quad - 568.556\eta^2 + 164.798\eta^3 - 27.0181\eta^4 + 1.91826\eta^5, & \eta \geq 1. \end{cases}$$

##### B. DISTANCE CORRECTION

Our distance correction is inspired by more general versions of the standard dipole and the relation between these diffusion dipoles and similar solutions from more exact transport theory. The main idea is to see how our model without the distance correction differs in terms of the distance between the points of incidence and emergence. We limit our investigation to the planar semi-infinite medium which is also the case that we considered when configuring the dipole.

Suppose we orient our coordinate system such that the  $xy$ -plane is the surface and the ray is incident at the origin with the  $z$ -axis along  $-\vec{n}_o$ . Assuming that the medium exhibits isotropic scattering and that the solution is independent of outgoing direction, the emergent radiance  $L_r(\mathbf{x}_o, \vec{\omega}_o)$  becomes an integral over  $z$  from 0 to  $\infty$  of a Hankel transform of a Green function which is Fourier transformed in the  $x$  and  $y$  coordinates [Williams 1982]. Analytical evaluation of a diffuse reflectance integral like this is difficult except in the special cases of a point source [Elliott 1955] and a ray source in the normal direction [Williams 2009]. In these two ‘‘monopole’’ solutions which incorporate a planar boundary, an approximate analytical evaluation of the diffuse reflectance integral is possible if the radial distance is corrected to

$$R^2 = r^2 + (z' + d_e)^2, \quad (32)$$

where  $z'$  is the depth of the point source or the internal ray source. For  $z' = 0$ , Elliott [1955] observed that the  $d_e^2$  term in Equation 32 essentially deals with the boundary in a way somewhat similar to what the standard dipole does. The main difference is that radial distance is corrected in the transport solution, whereas, in the standard dipole, the diffuse reflectance integral is approximated by displacing the real source ( $z' = z_r$ ) and mirroring it in an extrapolated boundary to place the virtual source (instead of  $d_e^2$ ). Our approach is motivated by this observation; we retain the extrapolated boundary by the virtual source, but we also introduce a radial distance correction for the real source.

It has been observed in work based on the diffusion dipole that the distance correction should change if the point of emergence is not in the tangent plane [Fretterd and Longini 1973] or if the ray is incident at an oblique angle [Wang and Jacques 1995]. The radial distance correction from transport theory (Equation 32) also needs modification in these cases, since  $z'$  and  $d_e$  are no longer taken in the same direction. Then, considering triangle geometry,

$$R^2 = r^2 + z'^2 + d_e^2 - 2z'd_e \cos \beta, \quad (33)$$

where we approximate  $\cos \beta$  as in Equation 25.

Considering Elliott's comparison of the transport solution and the diffusion dipole, we do not include the  $d_e^2$  term in our radial distance correction as this part is included with the virtual source. At oblique incidence, the diffuse reflectance integral can be reformulated as an integral along the refracted ray. This integral can be approximated to first order by choosing an offset  $D^*$  along the refracted ray. Then

$$z' = D^* |\mu_0| \quad \text{with} \quad \mu_0 = -\vec{\omega}_{12} \cdot \vec{n}_o, \quad (34)$$

where  $D^* = D$  if the surface is frontlit ( $\mu_0 > 0$ ) and  $D^* = 1/(3\sigma_t)$  if the surface is backlit ( $\mu_0 \leq 0$ ). The use of  $D^*$  instead of  $3D$  was determined empirically. Our corrected radial distance for the real source is then Equation 24, where we in the backlit case, due to some minor issues along sharp edges, decided to set the correction term as if light were normally incident with  $\mathbf{x}_o$  located along the normal direction (such that  $\mu_0 = -1$  and  $\cos \beta = \sin \theta = 0$ ).

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